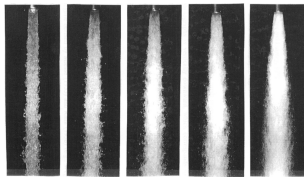


# Turbulence intensity's effect on liquid jet breakup from long circular pipes

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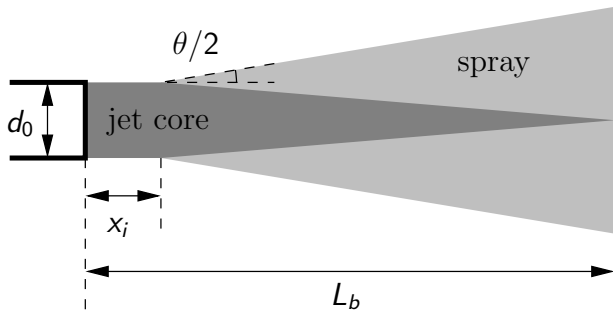
From P.-K. Wu (1992)

## Why pipe jets?

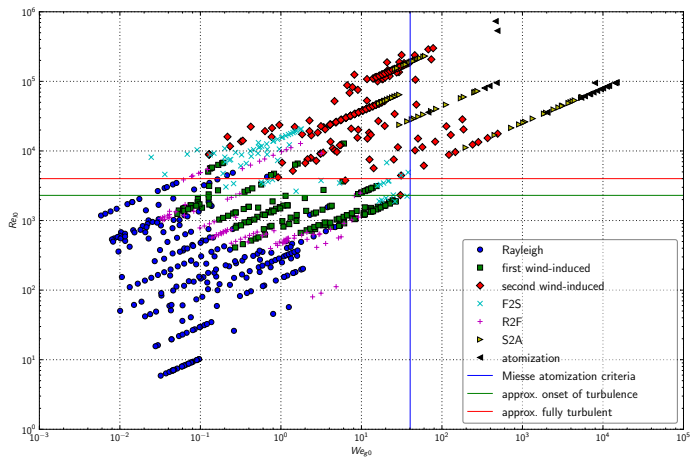
- ▶ Easy to set up
- ▶ Common in previous literature
- ▶ Universal flow state
- ▶ Problems with previous experiments:
  - ▶ confounding between variables:  $Re$  and  $We$ , and  $Re$  and  $Tu$
  - ▶ neglected an important quantity:  $Tu$
  - ▶ apples to oranges comparisons: need nozzle standardization to ensure that other variables (e.g., the integral scales, velocity profile, anisotropy) remain consistent
- ▶ Can estimate turbulence intensity from friction factor measurement:

$$Tu_0 = \frac{\sqrt{\frac{2}{3}k}}{U_0} = \frac{\sqrt{u'^2}}{U_0} = 0.36552f^{0.45867}$$

# Jet nomenclature



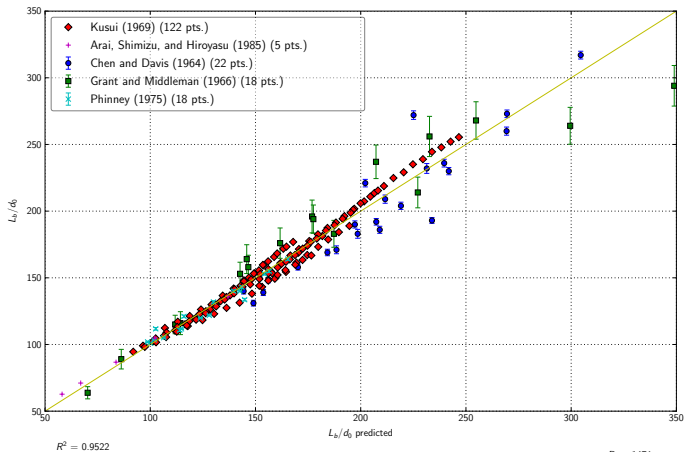
# Regime map



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# Breakup length

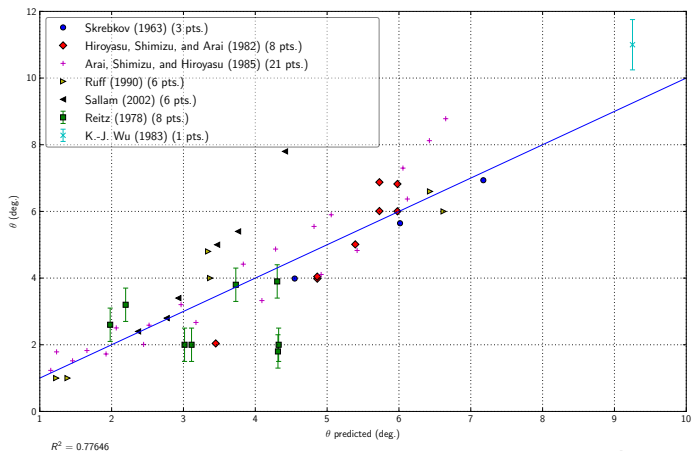
$$\frac{L_b}{d_0} = 3.1869 We_{\ell 0}^{0.3101} Re_{\ell 0}^{0.0207} Tu_0^{-0.2603} \left( \frac{\rho_\ell}{\rho_g} \right)^{0.02197}$$



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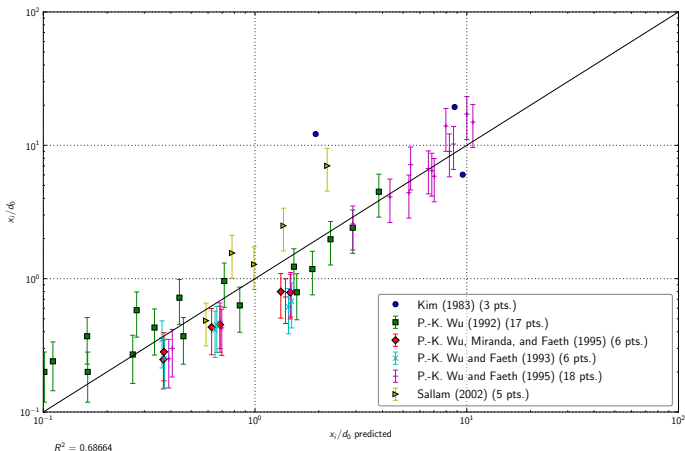
# Spray angle

$$\tan\left(\frac{\theta}{2}\right) = 0.007870 We_{\ell 0}^{0.4300} Re_{\ell 0}^{-0.0177} Tu_0^{0.7841} \left(\frac{\rho_{\ell}}{\rho_g}\right)^{-0.1488}$$



# Breakup onset location

$$\frac{x_i}{d_0} = 16.0298(We_{\ell 0} Tu_0^3)^{-0.9567}$$



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## Droplet size ( $D_{32}$ )

- ▶ Inverse scaling:  $D_{32}/d_0 \propto (We_{\ell 0} Tu_0^2)^{-1}$ 
  - ▶ Natanzon (1938), Bogdanovich (1948), Sitkei (1963), and Lebedev (1977)
  - ▶ Similar: Kerstein, Movaghar, and Oevermann (2017)
- ▶ Faeth group:  $D_{32}/d_0 \propto (We_{\ell 0} Tu_0^2)^{-3/5}$
- ▶ Me (nearly inverse):

$$\frac{D_{32}}{d_0} \propto (We_{\ell 0} Tu_{v0}^2 F_v)^{-1}$$

$F_v$  is a function of the integral scale-rms velocity Weber number and the ratio of minimum velocity to form a droplet to the rms velocity. (Minimum velocity: either Hinze or Kolmogorov velocity scale, whichever larger.)



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## Non-dimensionalization

$$Re = Re_{\ell,0} = \frac{\bar{U}_0 d_0}{\nu_\ell} \quad \text{nozzle liquid Reynolds number}$$

$$Fr = Fr_0 = \frac{\bar{U}_0^2}{gd_0} \quad \text{nozzle Froude number}$$

(kinetic energy to gravitational energy ratio)

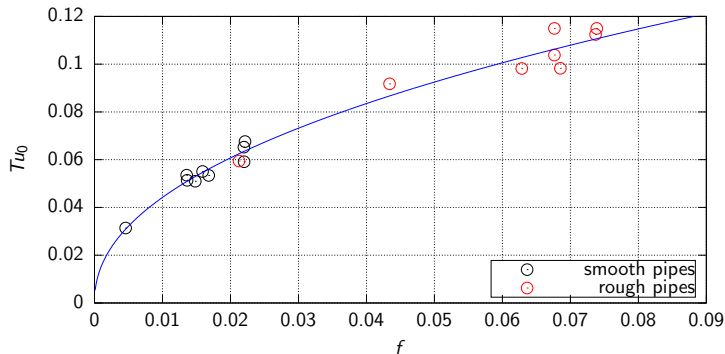
$$We = We_{\ell,0} = \frac{\rho_\ell \bar{U}_0^2 d_0}{\sigma} \quad \text{nozzle liquid Weber number}$$

(kinetic energy to surface energy ratio)

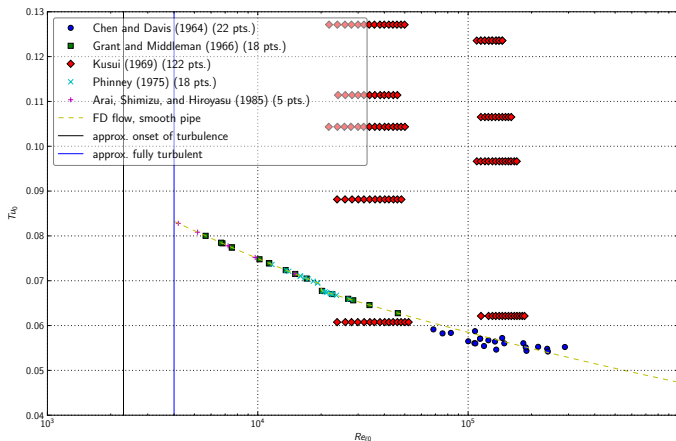
$$Tu = Tu_{\ell,0} = \frac{u'}{\bar{U}_0} \quad \text{turbulence intensity}$$

## Fully developed pipe $Tu$ correlation

$$Tu_0 = \frac{\sqrt{\frac{2}{3}k}}{U_0} = \frac{\sqrt{u'^2}}{U_0} = 0.36552f^{0.45867}$$



# Confounding example



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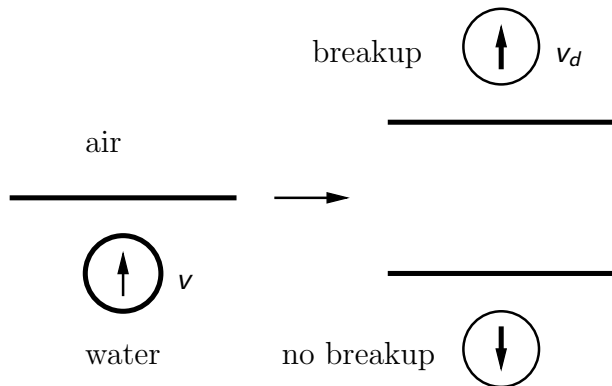
## Problems with pipe jets

- ▶  $Tu$  can be much higher than in practice (e.g., fire hose jets should have low  $Tu$ )
  - ▶ Some  $Tu > 0$  has been found to *stabilize* jets Sauerwein, 1992
- ▶ Harder to study transition in the jet rather than nozzle/pipe
- ▶  $Tu$  estimate may not be very precise (better than nothing!)
- ▶ Kusui (1969) not rough for entire length of tube

# Data compilation

- ▶ 21 studies (so far)
- ▶ 1027 data points:
  - ▶ 25.7% measured friction factors
  - ▶ 68.1% measured hydrodynamic regimes
  - ▶ 13.7% rough pipes
  - ▶  $We_{\ell 0} = 5.0 \cdot 10^0 - 1.9 \cdot 10^7$
  - ▶  $Re_{\ell 0} = 5.9 \cdot 10^0 - 1.0 \cdot 10^7$
  - ▶  $Tu_0 = 0.0 - 0.127$
  - ▶  $Fr_0 = 4.0 \cdot 10^0 - 2.3 \cdot 10^8$
  - ▶  $\rho_{\ell} / \rho_g = 19.0 \cdot 10^0 - 1.3 \cdot 10^5$
  - ▶  $Ma_g = 0.001 - 0.741$
  - ▶  $L_0 / d_0 = 16.8 - \approx 2200$
- ▶ Detail about experiment included as well: flow conditioning, nozzle outlet geometry, error estimates, photographic details, orientation of jet, vibration isolation, chamber diameter

## Model idea: conditioning on droplet formation



## “Ligament” model and energy balance for mean droplet size

Ligament model leads to:

$$v_d = v \left( 1 - \frac{6C_F}{\pi} \frac{\sigma}{\rho_\ell \ell v^2} \right)$$

Energy balance leads to:

$$\frac{6\sigma}{D_{32}} = \frac{1}{2} \rho_\ell v'^2 F_v$$

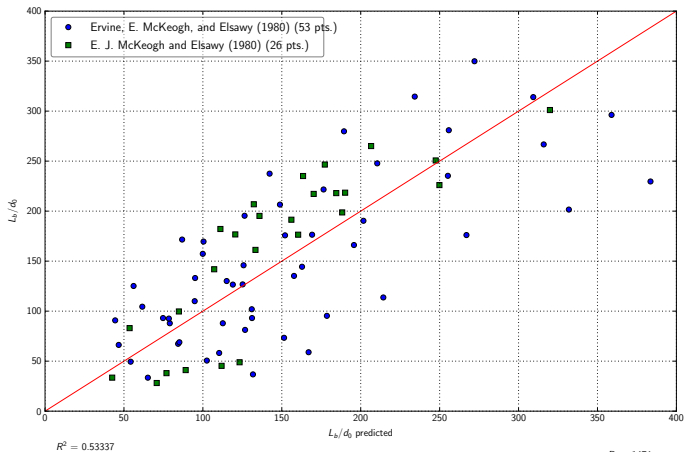
where  $F_v$  is a messy function determined by applying a conditional average to the ligament model, i.e.,  $\langle v_d^2 \mid v > v_{\min} \rangle$ , where  $v_{\min}$  is the minimum turbulent fluctuation velocity which can form a droplet (scales with Hinze scale or Kolmogorov scale).

Early work on turbulent energy balance for droplet formation:  
Natanzon (1938)



# Breakup length correlation compared against non-pipe jets

$$\frac{L_b}{d_0} = 3.1869 We_{\ell 0}^{0.3101} Re_{\ell 0}^{0.0207} Tu_0^{-0.2603} \left( \frac{\rho \ell}{\rho_g} \right)^{0.02197}$$



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## Breakup length model

Earlier theoretical work returned:

$$\frac{L_b}{d_0} \propto We^{1/3} Tu^{-1/3}$$

Compare with correlation from my data compilation (185 points):

$$\frac{L_b}{d_0} = 3.1869 We^{0.3101} Re^{0.0207} Tu^{-0.2603} \left( \frac{\rho_\ell}{\rho_g} \right)^{0.02197}$$

One-third scaling is a consequence of inertial range and should only apply in the “second wind-induced regime” (hypothesis at the moment).

Justification of this model earlier was sketchy, now I can see how it can be justified via my conditional process. Needs to be fleshed out, however.

# Takeaways

- ▶ Use tubes of varying roughness to easily control  $Tu$  independent of  $Re$  in jet breakup experiments
- ▶ Use tubes of multiple diameters to avoid confounding of  $Re$  and  $We$
- ▶ Read more foreign language papers!

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